

# Optimisation of Methanol Synthesis by CO<sub>2</sub> Hydrogenation

Chikamso Anthony Nwani  
 Department of Chemical and Petroleum Engineering  
 University of Lagos, Nigeria

## Background & Description:

Carbon dioxide (CO<sub>2</sub>) is one of greenhouse gases, which can cause global warming. To combat the problem of CO<sub>2</sub> emissions, present day studies show that methanol show be considered as a suitable product because of its use in various petroleum based-liquid fuels.

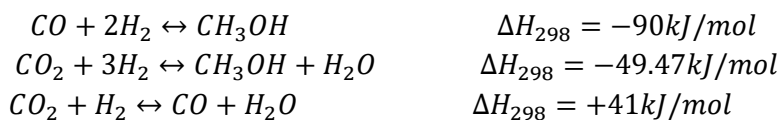
Here, simulation carried out for a process which converts hydrogenates CO<sub>2</sub> into methanol. A plug flow reactor (PFR) is used to react hydrogen with the carbon dioxide in the synthesis gas to produce methanol.

The traditional syngas process has been explored exhaustively in literature and to make methanol production via CO<sub>2</sub> hydrogenation a competitive process, the optimal operating conditions with minimum production cost are considered. This new process can be considered a green process because it uses CO<sub>2</sub> obtained from thermal plants, stacks etc as the raw material contributing to the mitigation of CO<sub>2</sub> emissions. This thesis studied optimization of methanol production via CO<sub>2</sub> hydrogenation using multiple design variables. The objective function of this optimization was to maximize the profit of methanol production.

## Flowsheet Description

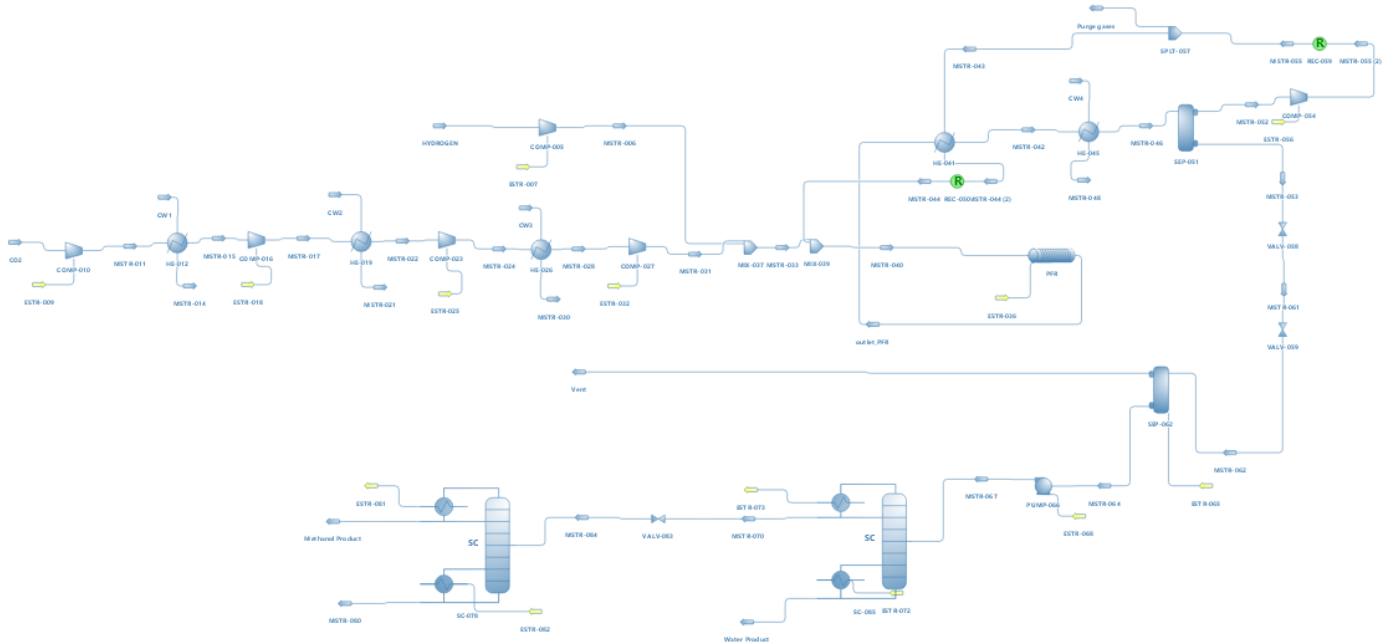
Here, fixed amounts of CO<sub>2</sub> and hydrogen in different streams is used for feed. In process, “Peng-Robinson” property model is used. Vanden Bussche and Froment’s (Vanden Bussche, et al., 1996) kinetic model was used taking only the water-gas-shift reaction and the CO<sub>2</sub> hydrogenation into consideration. The process can be divided into four sections:

- (1) Compression and Reactor Preheating
- (2) Reactor (PFR)
- (3) Separator, Recycle, and Vent
- (4) Flash and Distillation



In this process, the feed of 1,000 kmoles per hour of carbon dioxide at 40°C and 20 bar was mixed with the 3,000 kmoles per hour of hydrogen (at the same conditions). The mixture was then compressed, heated and sent to the first equilibrium reactor. The first reactor partially converted CO<sub>2</sub> to methanol as liquid product. The unreacted CO<sub>2</sub> and H<sub>2</sub> then entered the second equilibrium reactor to produce more methanol product. The pressure of gas phase leaving the second reactor was reduced to recover methanol as liquid phase. All liquid methanol products were sent to the first distillation column, where the light components (CO, CO<sub>2</sub>, and H<sub>2</sub>) leaved at the top of the column. The mixture of methanol and water leaved the column at the bottom and entered the second distillation column, where the methanol product with purity of 99.5% mole was obtained at the top of the column. The efficiency of the pumps and compressors was assumed at 75% (adiabatic). The specifications of the shortcut column were condenser temperature at 40.1°C and reflux ratio at 0.5. The specifications of the methanol distillation column was set at 99 %mole methanol product purity.

**Flowsheet:**



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**Results:**

- From the simulation, high pure methanol is obtained about (99%) at rate of 27 kg/hr as a top product and water as bottom product at rate of 47.5 kg/h.
- In the plug flow reactor (PFR), about 57% and 19% conversion of carbon monoxide and carbon dioxide is achieved respectively.

The Nelder-Mead simplex constrained solving method was applied to optimize the objective function model for the maximum generated profit. In the optimal region of study, the inlet pressure of the hydrogen stream, inlet pressure and temperature to the reactor show significant impacts on the methanol production rate. The obtained maximized methanol production plant profit from a base value of Current value of \$1068.65 was **\$1460.12/hr of produced methanol**

The objective function is thus given as

$$Max P = C_{MeOH}P_{MeOH} + C_{vent}P_{vent} + C_{purge}P_{purge} - C_{H2}P_{H2} - C_{CO2}P_{CO2} - \sum C_{cw}P_{cw}$$

$$P = 0.343 * x1 + 0.24 * x2 + 8.14 * x3 - 1.88 * x4 - 3.5 * x5 - 0.1 * (cw1 + cw2 + cw3 + cw4)$$

**Table 1: shows the constraints and initial value to maximize the profit (\$/hr) generated from the methanol production plant via CO<sub>2</sub> hydrogenation.**

| Name | Object           | Lower Limit | Upper Limit | Initial Value | Unit |
|------|------------------|-------------|-------------|---------------|------|
| x1   | Methanol Product | 40          | 100         | 48.0074       | kg/h |
| x2   | Vent             | 20          | 50          | 25.1293       | kg/h |
| x3   | Purge gases      | 400         | 500         | 453.376       | kg/h |
| x4   | HYDROGEN         | 100         | 400         | 105.46        | kg/h |
| x5   | CO <sub>2</sub>  | 200         | 400         | 258.646       | kg/h |
| cw1  | MSTR-013         | 3500        | 4000        | 3600          | kg/h |
| cw2  | MSTR-020         | 3500        | 4000        | 3600          | kg/h |
| cw3  | MSTR-029         | 3500        | 4000        | 3600          | kg/h |
| cw4  | MSTR-047         | 3500        | 4000        | 3600          | kg/h |

**Table 2 shows the local optimal operating conditions to maximize the profit (\$/hr) generated from the methanol production plant via CO<sub>2</sub> hydrogenation.**

| Parameters                 | Optimal values | Units |
|----------------------------|----------------|-------|
| Methanol Product, x1       | 99.99          | Kg/hr |
| Vent stream, x2            | 22.215         | Kg/hr |
| Purge stream, x3           | 456.89         | Kg/hr |
| H <sub>2</sub> stream, x4  | 105.46         | Kg/hr |
| CO <sub>2</sub> stream, x5 | 256.646        | Kg/hr |
| Cooling water, cw1         | 3600           | Kg/hr |
| Cooling water, cw2         | 3600           | Kg/hr |
| Cooling water, cw3         | 3600           | Kg/hr |
| Cooling water, cw4         | 3600           | Kg/hr |